

544/ Copy 1

NUWC-NPT Reprint Report 10,860  
20 October 1997

# Large-Signal Characterization of PMN-PT-Ba (90/10/3)

Robert S. Janus  
Mark B. Moffett  
James M. Powers  
Submarine Sonar Department

LIBRARY USE ONLY



**Naval Undersea Warfare Center Division  
Newport, Rhode Island**

Approved for public release; distribution is unlimited. Reprint  
of a poster presentation made at the 1997 *ONR PMN Measurement  
Workshop*, 9 October 1997, Alfred, NY.

Report Documentation Page			Form Approved OMB No. 0704-0188	
Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.				
1. REPORT DATE <b>20 OCT 1997</b>		2. REPORT TYPE		3. DATES COVERED <b>20-10-1997 to 20-10-1997</b>
4. TITLE AND SUBTITLE <b>Large-Signal Characterization of PMN-PT-Ba (90/10/3)</b>		5a. CONTRACT NUMBER		
		5b. GRANT NUMBER		
		5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S) <b>Robert Janus; Mark Moffett; James Powers</b>		5d. PROJECT NUMBER		
		5e. TASK NUMBER		
		5f. WORK UNIT NUMBER		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) <b>Naval Undersea Warfare Center Division,1176 Howell Street,Newport,RI,02841-1708</b>		8. PERFORMING ORGANIZATION REPORT NUMBER <b>RR 10,860</b>		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) <b>Office of Naval Research</b>		10. SPONSOR/MONITOR'S ACRONYM(S) <b>ONR</b>		
		11. SPONSOR/MONITOR'S REPORT NUMBER(S)		
12. DISTRIBUTION/AVAILABILITY STATEMENT <b>Approved for public release; distribution unlimited</b>				
13. SUPPLEMENTARY NOTES <b>NUWC2015 Reprint of a poster presentation made at the 1997 ONR PMN Measurement Workshop, 9 October 1997, Alfred, NY.</b>				
14. ABSTRACT <b>Large-signal measurements are reported for the relaxor ferroelectric, lead magnesium niobate-lead titanate (PMN-PT-Ba, 90/10/3), manufactured by Lockheed-Martin. The material has been formulated to produce optimal performance at 5 degrees Centigrade for application in sonar transducers. Charge and strain measurements were taken at 5?? and 23?? C on a material sample (2x2x10mm) mechanically loaded with 2, 4, 6, 8, and 10 ksi of compressive stress. The sample was electrically dc biased and driven with 5 cycle, 10 Hz pulses to a peak electric field of 2 MV/m. Values for the piezoelectric coefficient, d33, electrical permittivity, E33T, and elastic compliance, S33E, were computed from the measurement data. These three parameters determine the coupling factor, k33, which indicates the effectiveness of the material to convert electrical energy to mechanical energy. For the mechanical loads considered, k33 varied from 0.49 to 0.51 at 5?? C, and from 0.44 to 0.49 at 23?? C.</b>				
15. SUBJECT TERMS <b>PMN-PT-Ba, 90/10/3; sonar transducers</b>				
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT <b>Same as Report (SAR)</b>	18. NUMBER OF PAGES <b>13</b>
a. REPORT <b>unclassified</b>	b. ABSTRACT <b>unclassified</b>	c. THIS PAGE <b>unclassified</b>		



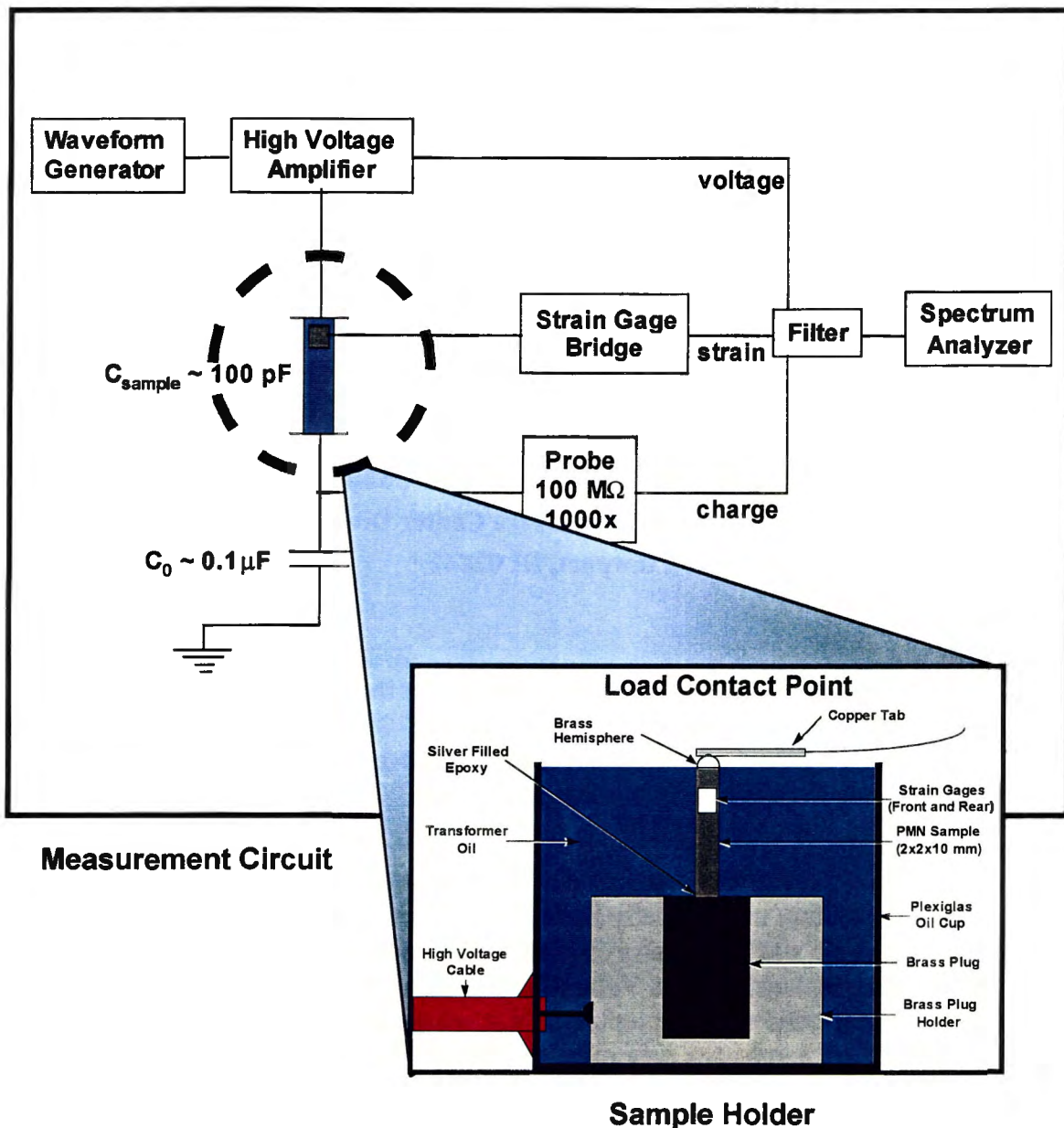
# **LARGE-SIGNAL CHARACTERIZATION OF PMN-PT-Ba (90/10/3)**

**Robert S. Janus, Mark B. Moffett, and James M. Powers**  
**Naval Undersea Warfare Center Division**  
**Newport, RI 02841**

Large-signal measurements are reported for the relaxor ferroelectric, lead magnesium niobate - lead titanate (PMN-PT-Ba, 90/10/3), manufactured by Lockheed-Martin. The material has been formulated to produce optimal performance at 5° Centigrade for application in sonar transducers.

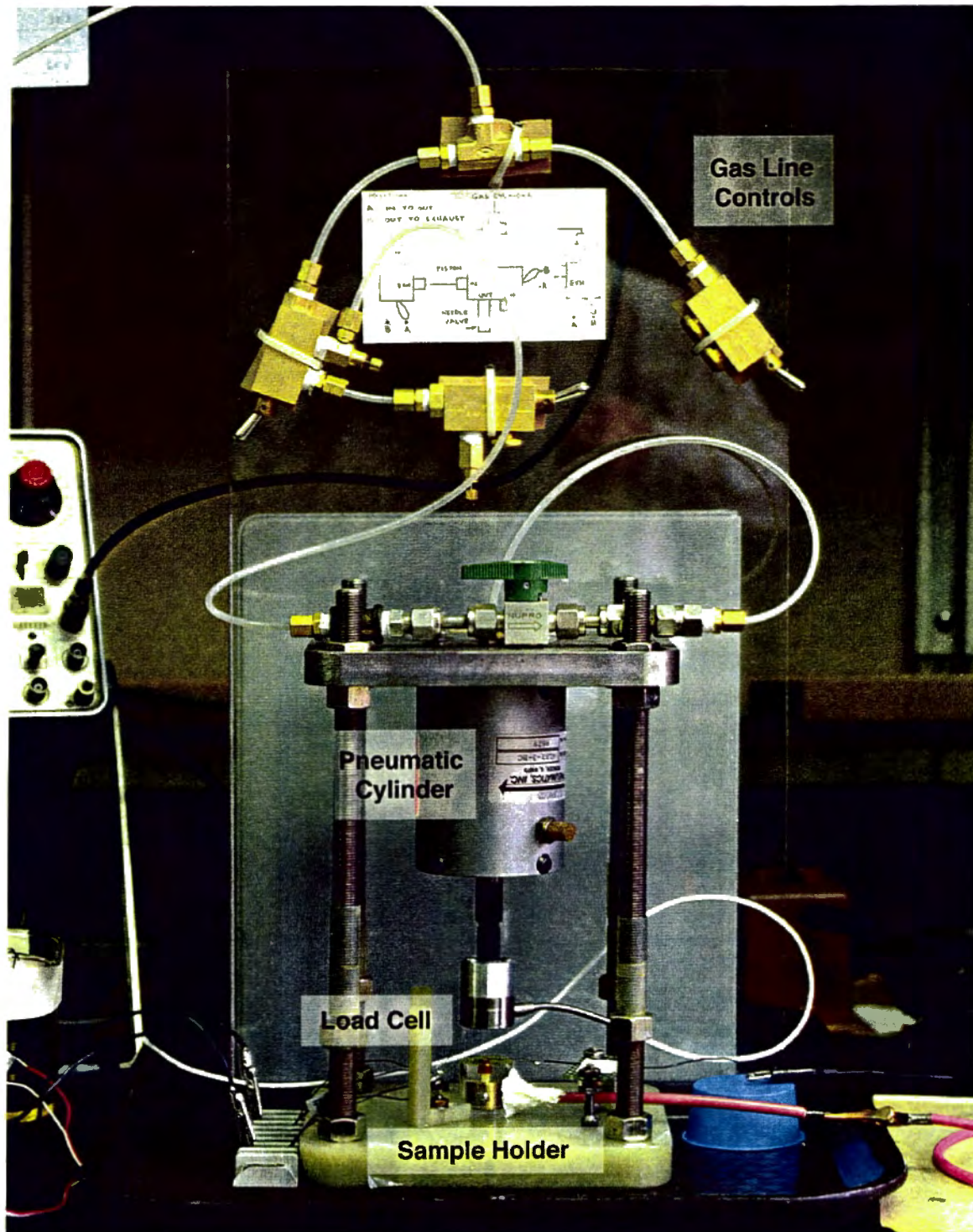
Charge and strain measurements were taken at 5° and 23° C on a material sample (2x2x10 mm) mechanically loaded with 2, 4, 6, 8, and 10 ksi of compressive stress. The sample was electrically dc biased and driven with 5 cycle, 10 Hz pulses to a peak electric field of 2 MV/m. Values for the piezoelectric coefficient,  $d_{33}$ , electrical permittivity,  $\epsilon_{33}^T$ , and elastic compliance,  $s_{33}^E$ , were computed from the measurement data. These three parameters determine the coupling factor,  $k_{33}$ , which indicates the effectiveness of the material to convert electrical energy to mechanical energy. For the mechanical loads considered,  $k_{33}$  varied from 0.49 to 0.51 at 5° C, and from 0.44 to 0.49 at 23° C.

This work was supported by the Office of Naval Research (Code 332) and by Program Executive Officer, Undersea Warfare, Advanced Systems and Technology Office (PEO-USW-ASTO).

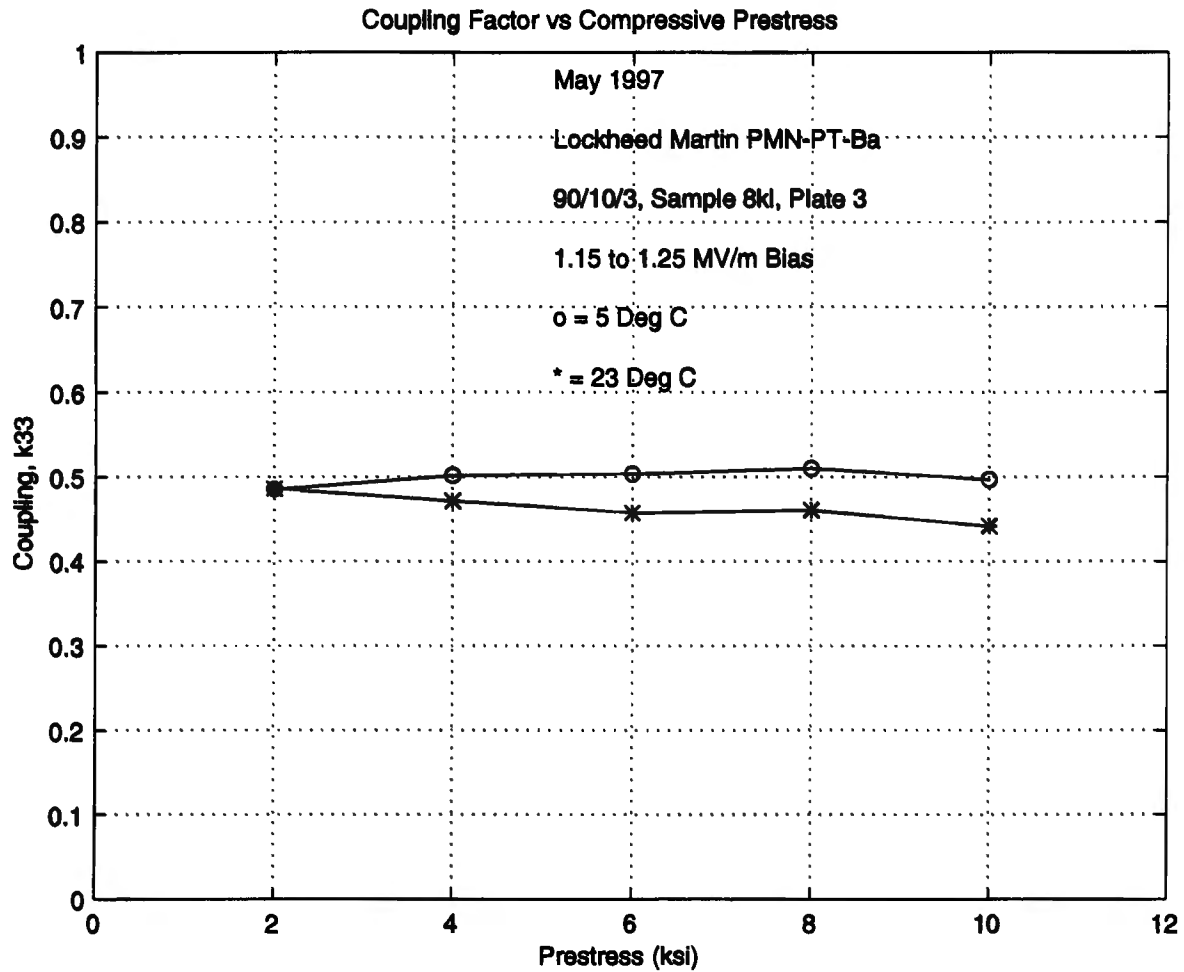


Because the capacitance (i.e., electrical permittivity) of the test sample changes with electric field level, the electrical charge on the sample is determined by measuring the voltage,  $V_0$ , across a fixed capacitor,  $C_0$ , that is in series with the sample. This configuration is the basic Sawyer-Tower circuit that is commonly employed for such measurements. The charges,  $Q_{\text{SAMPLE}}$  and  $Q_0$ , on the capacitors are equal, i.e.,  $Q_{\text{SAMPLE}} = Q_0 = C_0 V_0$ . For  $C_0 \gg C_{\text{SAMPLE}}$  nearly all the voltage,  $V_{\text{TOTAL}}$ , appears across  $C_{\text{SAMPLE}}$ .

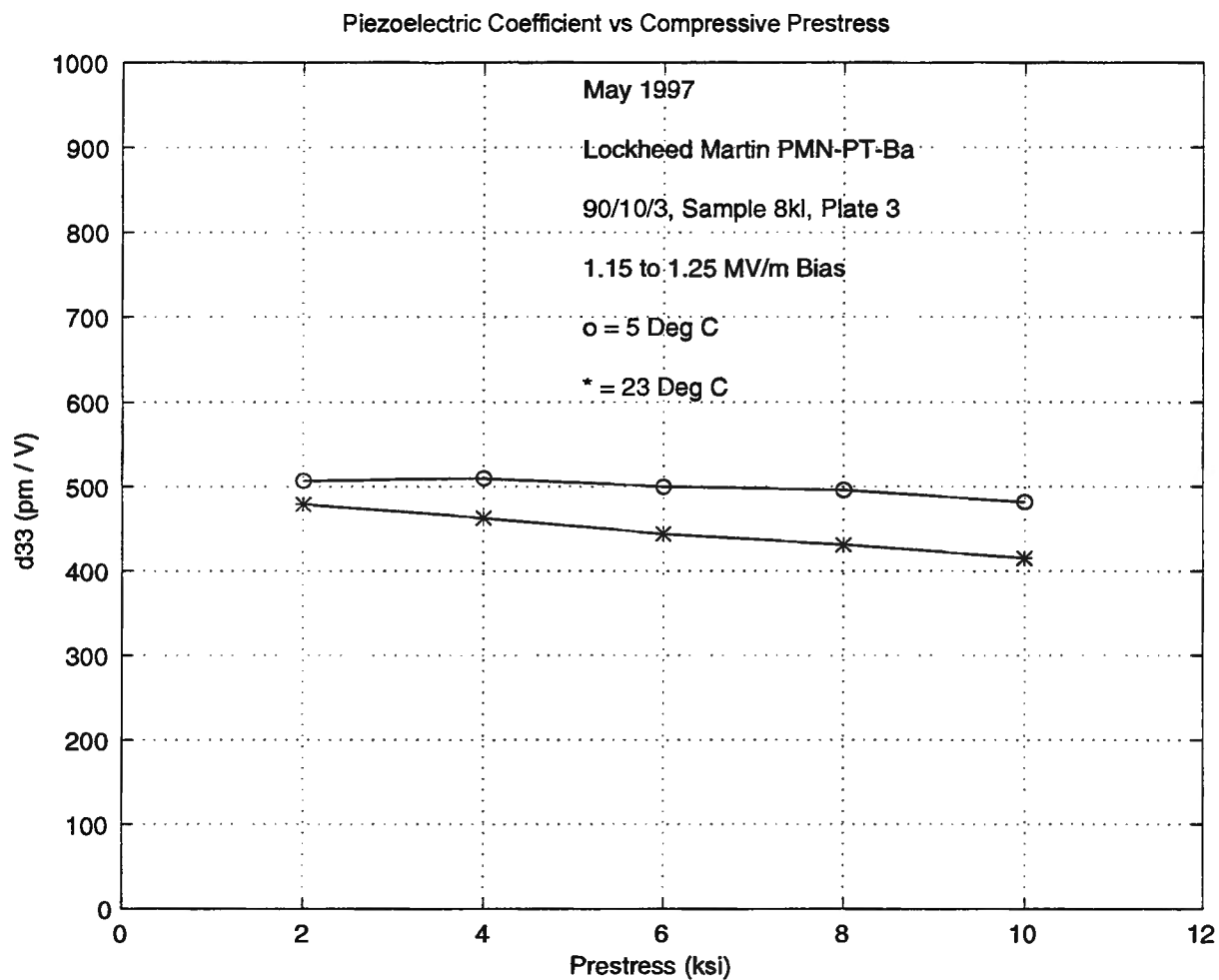
Strain data are obtained from two foil strain gages mounted on opposite sides of the sample. The two gages are wired together in series to cancel out bending strain components. Before connecting the gages in series, the individual outputs of both gages are simultaneously compared to assure that the applied mechanical load is uniformly distributed to minimize bending. Adjustment of the load is accomplished by moving the brass hemisphere that sits on top on the sample.



The mechanical bias is applied with a pneumatic cylinder which has a stiffness much less than that of the test sample. To reduce sliding friction, this cylinder has a "Rolling Diaphragm" rather than a conventional piston seal. The piston rod travels on a linear ball bushing to further minimize friction. Mechanical bias is monitored with the load cell.

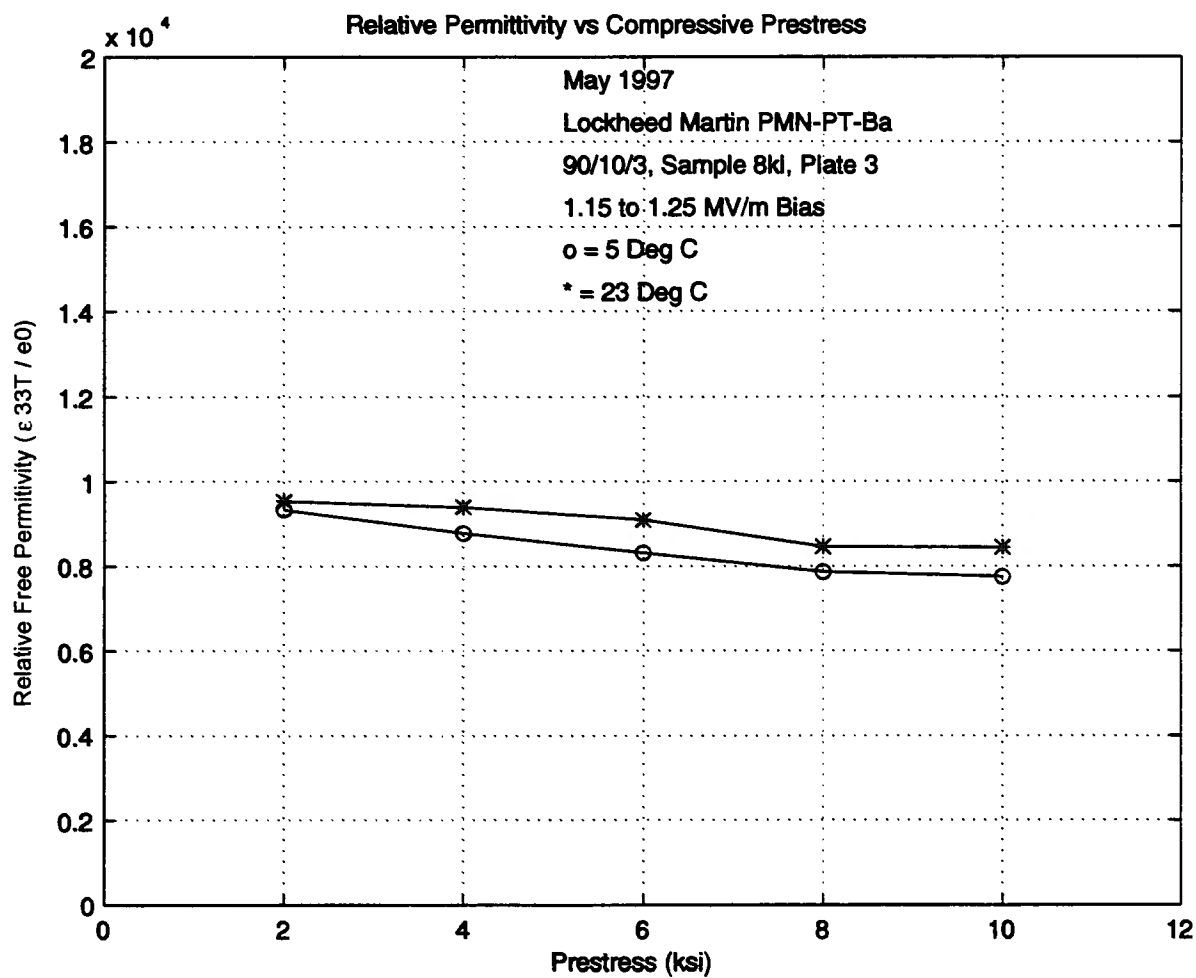


This plot summarizes the variation in coupling coefficient,  $k_{33}$ , with compressive stress. The results demonstrate that this material achieves a large-signal coupling factor,  $k_{33}$ , between 0.49 and 0.51 at the temperature at which it was designed to operate, 5° C. When compared with the data at 23° C,  $k_{33}$  is shown to be slightly enhanced at this lower temperature.

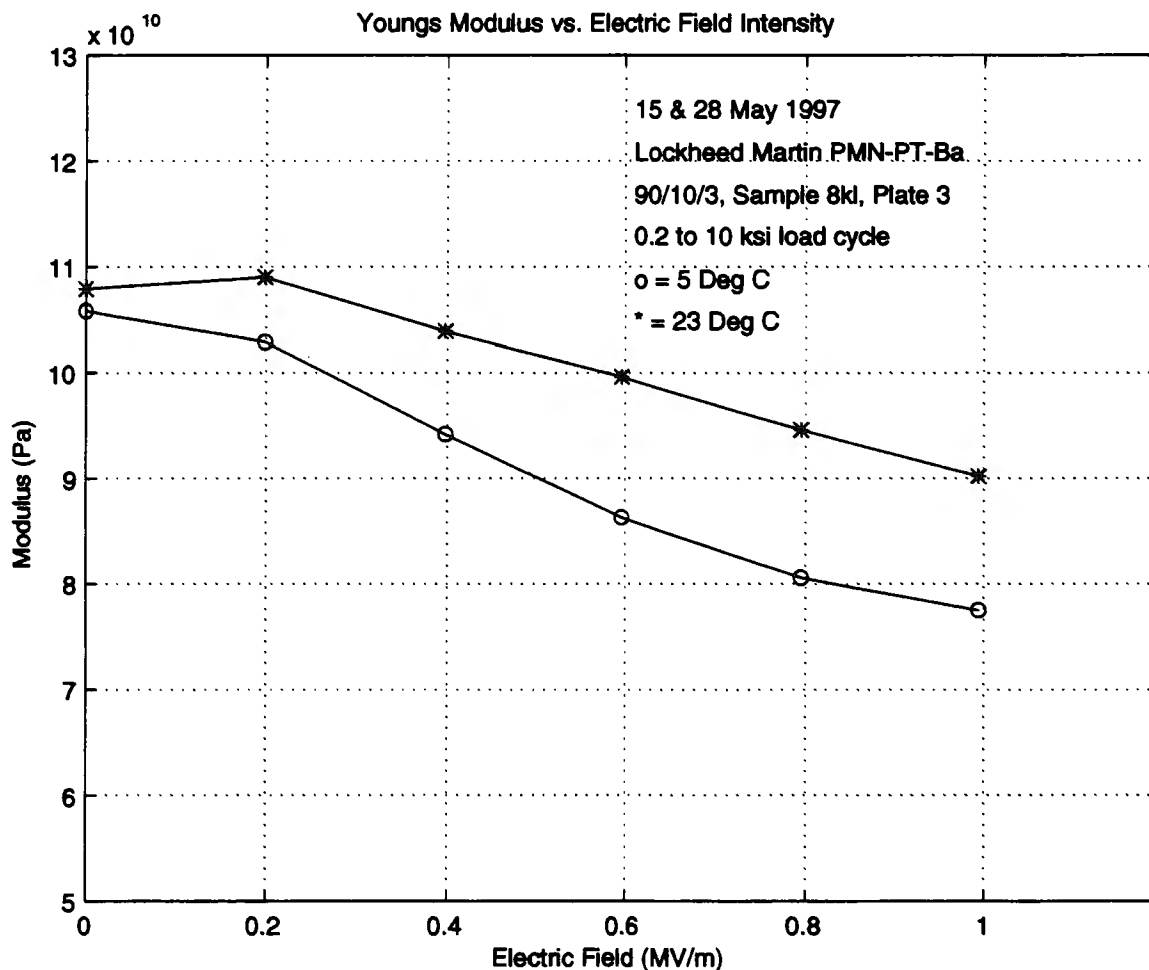


$k_{33}$  is derived from the piezoelectric coefficient,  $d_{33}$ , elastic compliance,  $s_{33}^E$ , and electrical permittivity,  $\epsilon_{33}^T$ :  $k_{33}^2 = d_{33}^2 / (s_{33}^E \epsilon_{33}^T)$ . Values for these three parameters that were used to compute the corresponding  $k_{33}$  are shown in this and the two following plots.

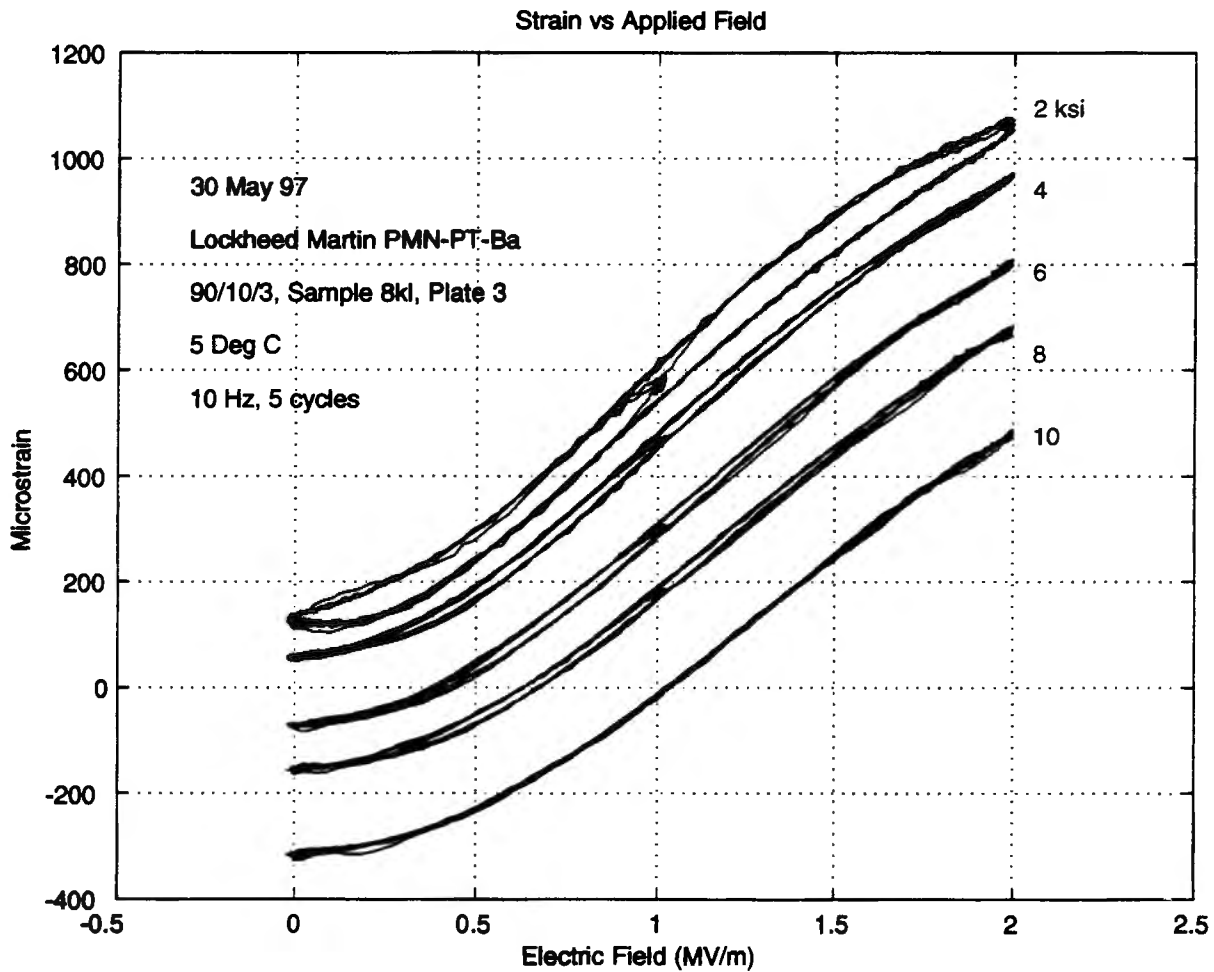




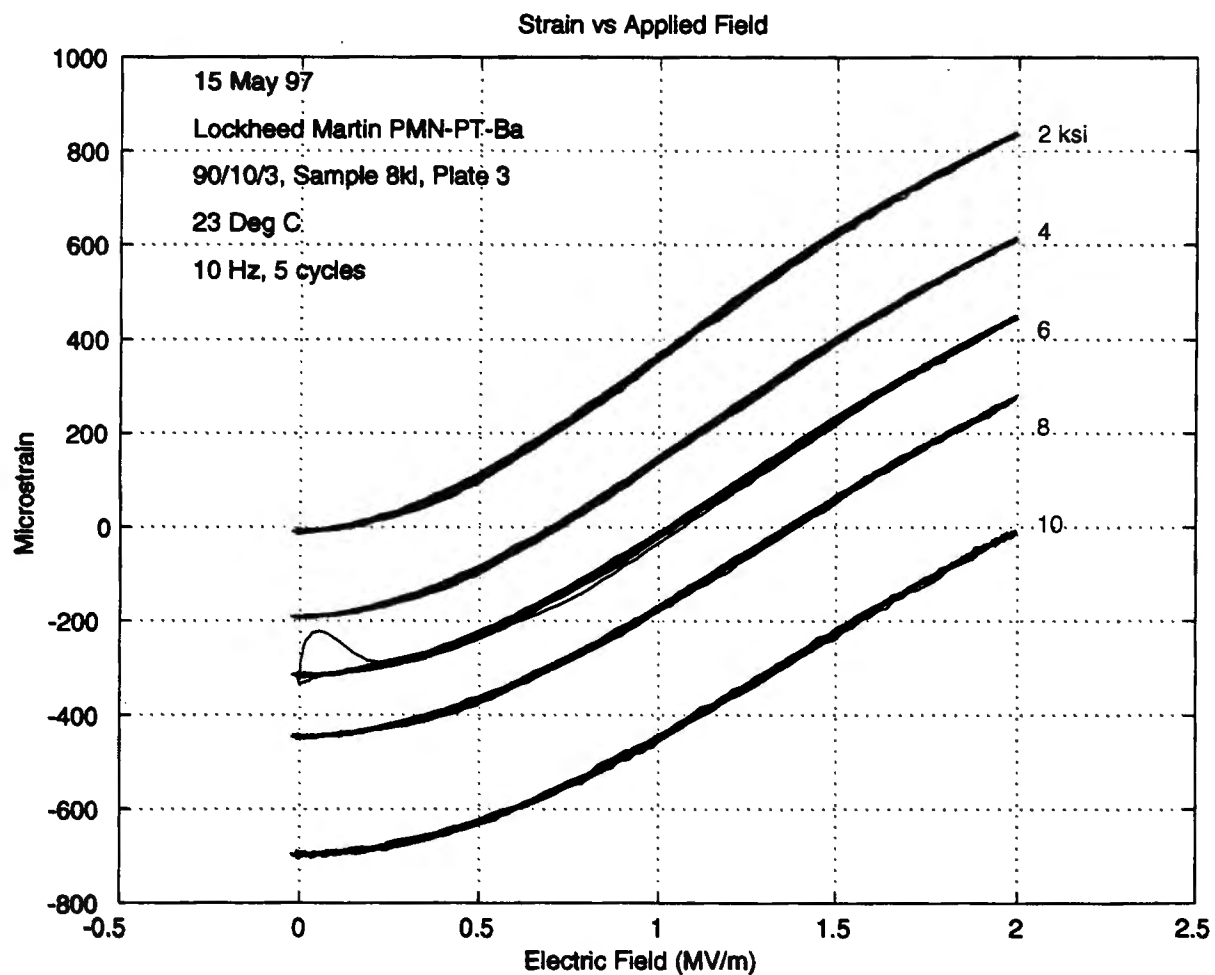
Here  $\epsilon_{33}^T$  has been normalized by the permittivity of free space,  $\epsilon_0$ .



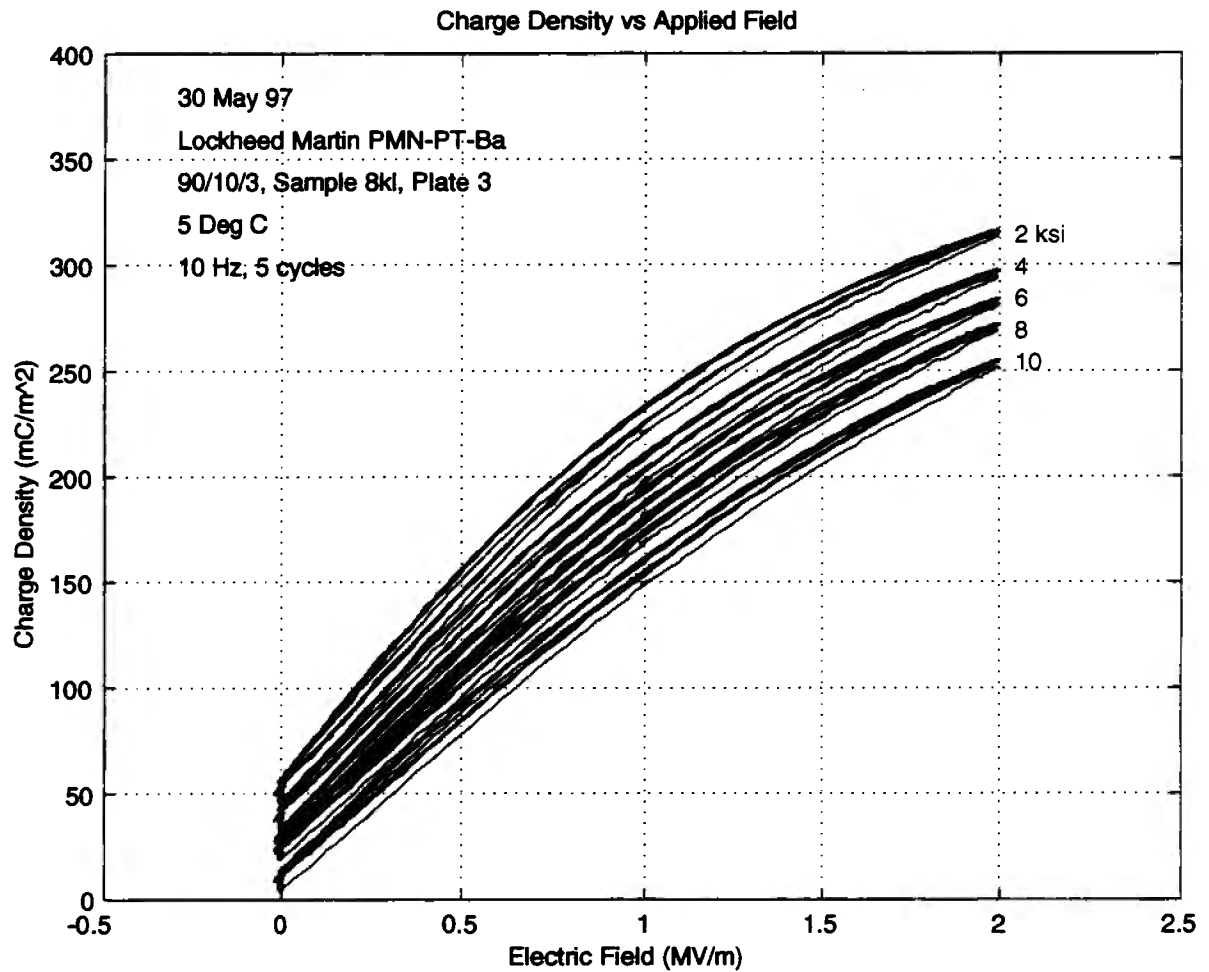
The line pressure to the pneumatic cylinder was ramped up and down to sweep the mechanical bias between 0.2 and 10 ksi while maintaining a constant electric field across the sample. Stress and strain data were simultaneously recorded and plotted against each other to obtain Young's modulus (i.e.,  $1 / s_{33}^E$ ). The resultant values of Young's modulus versus electric field are shown in this plot.



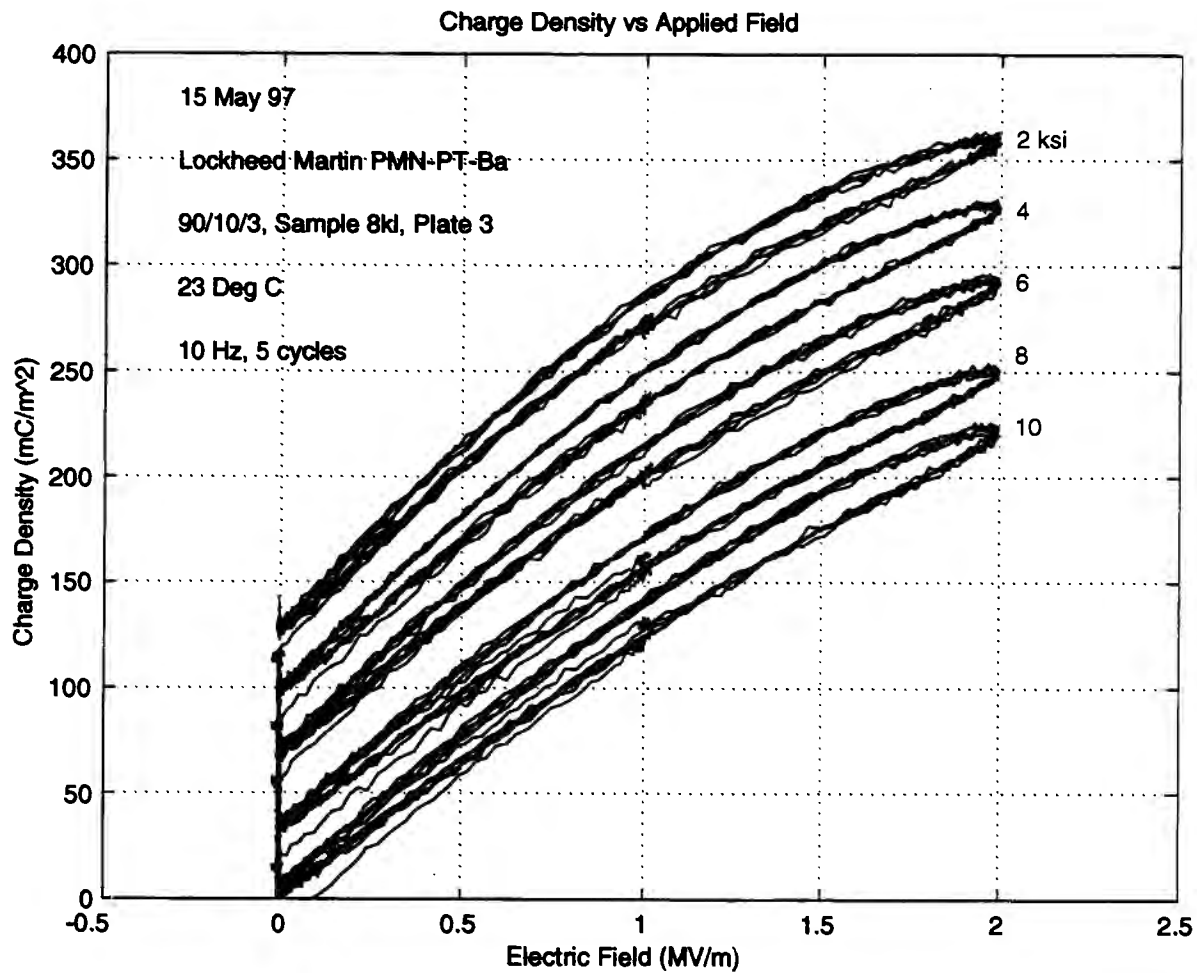
The PMN sample was driven with 5 cycle, 10 Hz sinusoidal pulses on a 1 MV/m dc pedestal to reach a peak field of 2 MV/m. The values of  $d_{33}$  were computed from the slopes of the hysteresis loops of strain,  $S_3$ , versus electric field,  $E_3$ ,  $d_{33} = \Delta S_3 / \Delta E_3$ . This is a composite plot of the loops taken at 5° C for prestresses of 2, 4, 6, 8, and 10 ksi. The slopes were determined between the endpoints at 0.5 and 2 MV/m. These large signal data represent the drive levels that are required for actual sonar operation.



This second set of strain versus field loops was taken to determine  $d_{33}$  at 23° C. Each loop is averaged from 10 data records.



$\epsilon_{33}^T$  is equal to the slope of the charge density,  $D_3$ , versus  $E_3$  loops,  $\epsilon_{33}^T = \Delta D_3 / \Delta E_3$ . This is a composite plot of the 2, 4, 6, 8, and 10 ksi data at 5° C. The slopes were determined between the end points at 0.5 and 2 MV/m. The loops have been offset for clarity.



These charge loops at 23° C are more open than their 5° C counterparts. This may indicate that the material has more dielectric loss at 23° C than at 5° C, its design temperature.

# CONCLUSIONS

- **Successfully measured coupling factor under high field ( $\leq 2$  MV/m) and high prestress ( $\leq 10$  ksi)**
- **Large-signal coupling factors (0.49 to 0.51) at 5° C for PMN-PT-Ba, 90/10/3 equal or exceed corresponding values measured at room temperature (23°C)**
- **Coupling factor varied with compressive stress by 4% and 10% at 5° and 23°C, respectively.**